



IEEE 1588 Timing Performance Under Environmental Stress in O-RAN Nodes

Gary Giust, PhD – Sr Mgr Technical Marketing
Jagdeep Bal – Dir Customer Engineering



Agenda

- Impact of oscillator performance in PTP time error
- O-RAN O-RU test setup and results
- Oscillator selection

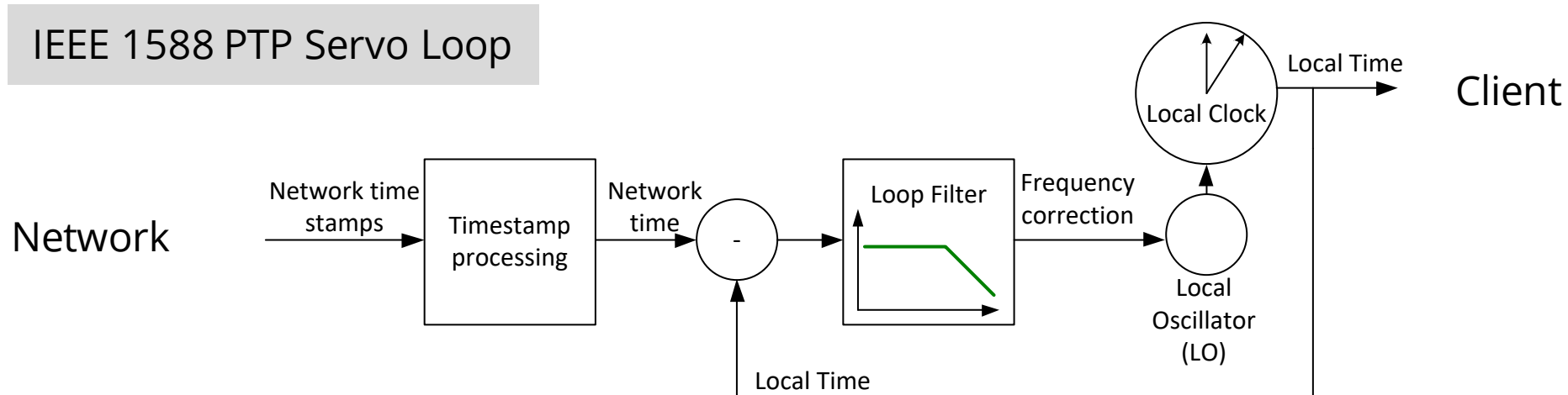
Proper Oscillator Selection is Necessary for Time/Phase Compliance

- Applies to all use cases with tight time/phase requirements
- Ensure quality by-design
 - Oscillator Performance
 - Proper loop filter design
 - Temperature profile
- Avoid over-specifying oscillator
 - OCXO vs TCXO
 - Higher cost, power, size, startup time, etc.

Key Standards Impacted by Oscillator Performance

- Network requirements
 - ITU-T G.8271.1 – Full timing support (FTS)
 - ITU-T G.8271.2 – Partial timing support (PTS)
 - O-RAN-WG4.CUS.0-v08.00 – Open fronthaul interfaces
- Clock specifications
 - ITU-T G.8273.2 – T-BC and T-TSC with FTS, variable temperature
 - dTE_L MTIE = 40, 40, ffs and ffs ns p-p for class A, B, C and D, respectively
 - ITU-T G.8273.4 – T-BC & T-TSC with PTS
 - dTE_L = 50 ns p-p assisted
 - dTE_L = 200 ns p-p unassisted
 - O-RAN Appendix H, O-DU time-error budget analysis
 - $|dTE_{L+H}| = \pm 45$ ns and ± 57 ns for class A and B, respectively

IEEE 1588 – Lower Oscillator $\Delta F/\Delta T$ Enables More Accurate Time Stamps



- In locked state, reducing loop-bandwidth...
 - filters more noise from input (network), but
 - increases noise from LO
- The optimal setting balances the two noise contributions.
- Thus, using a **lower-noise LO** enables the bandwidth to reduce, filtering more network noise, enabling
 - **more accurate time stamps**, or
 - **additional hops** in fronthaul network
- dF/dT performance is dominant oscillator noise source

Thermal Profile Greatly Influences PTP Time Error

ITU-T G.8263 – Timing characteristics of packet-based equipment clocks

Where variable temperature testing is required, it should be conducted using the temperature profile shown in Figure IV.1.

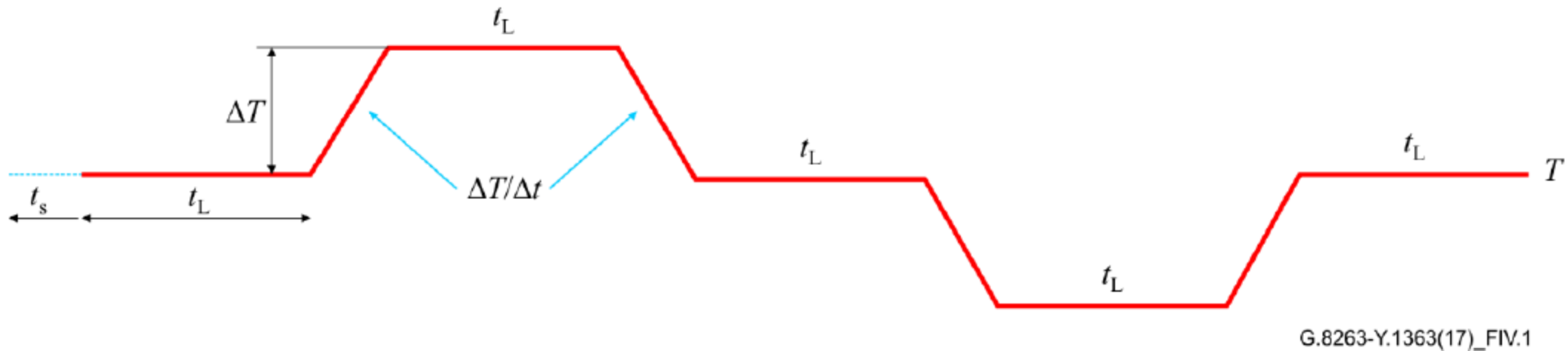
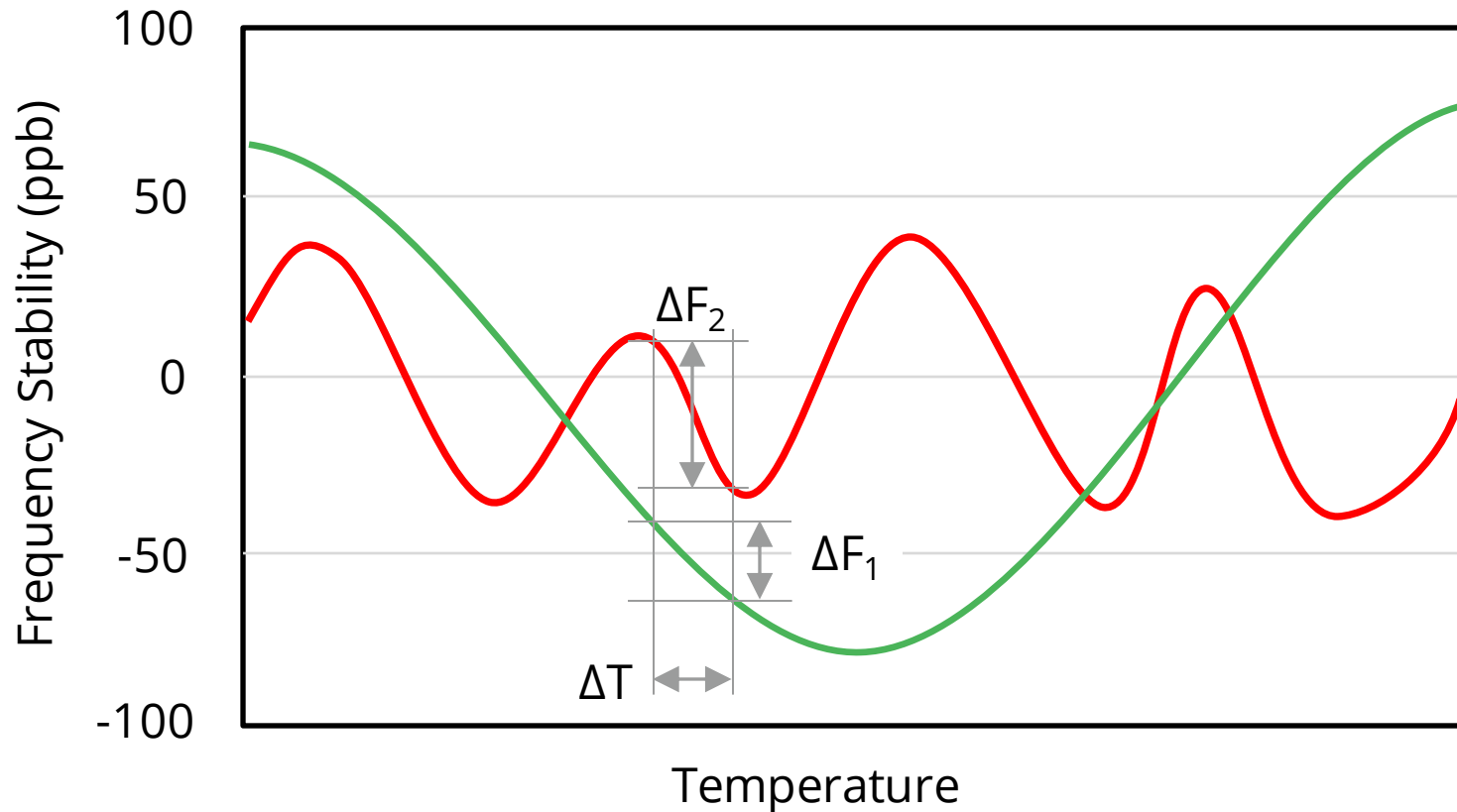


Figure IV.1 – Temperature profile

Smoother Frequency Change Matters More than Rated Lifetime Stability

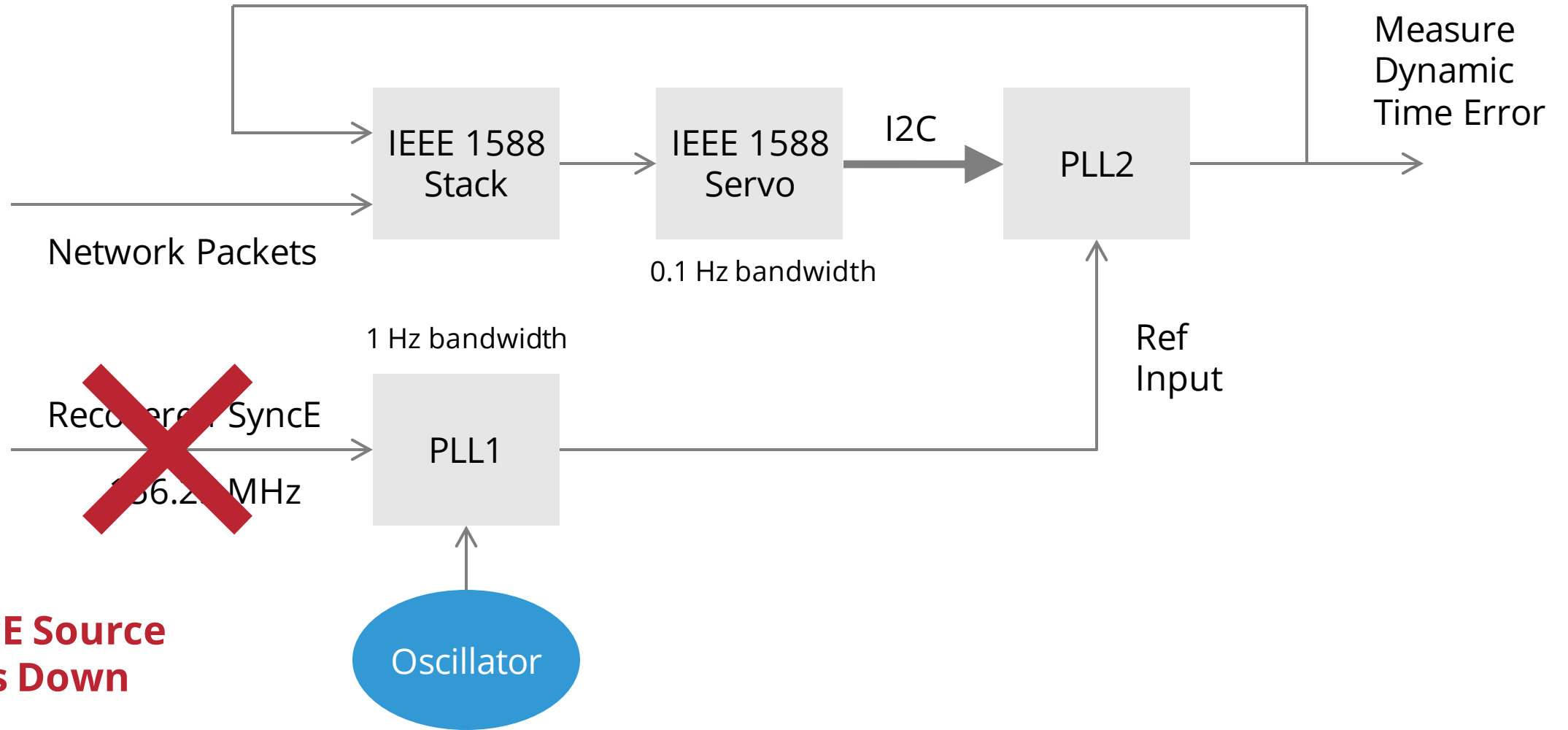


Device 1

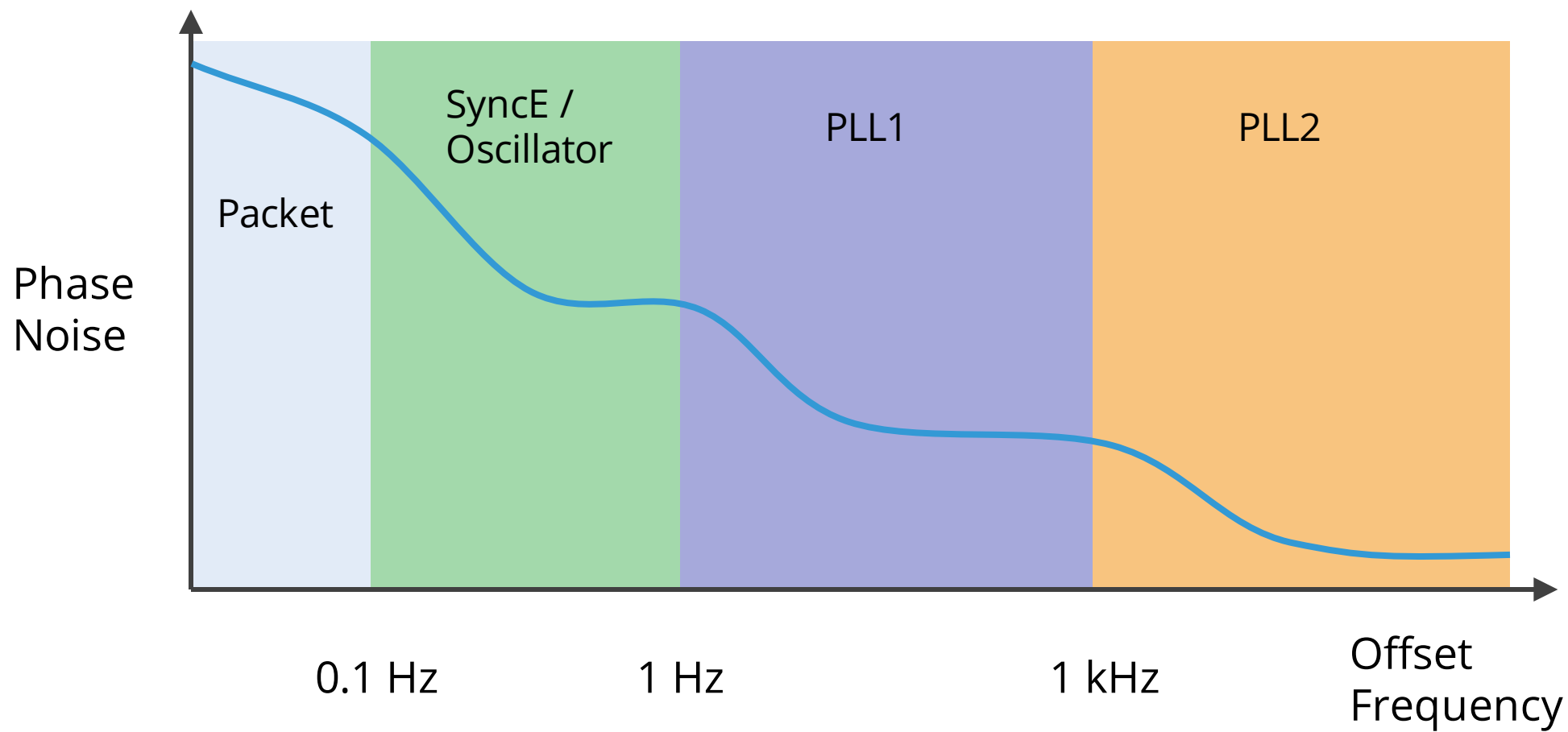
Which device is "better"?

Device 2

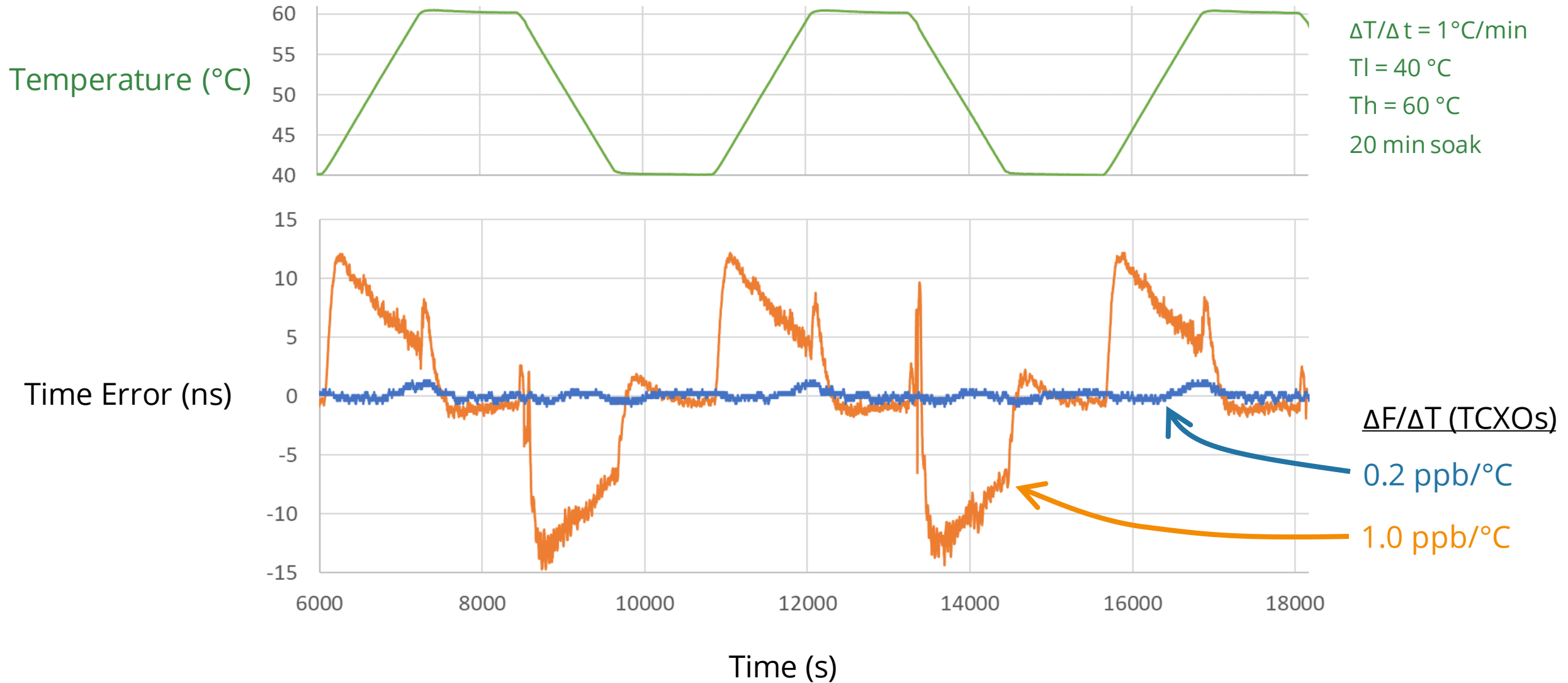
O-RU Test Setup – G.8275.1 Full Timing Support



Oscillator Contribution to Phase Noise



Thermal Profile Converts Oscillator $\Delta F/\Delta T$ to PTP Time Error



Lower Oscillator $\Delta F/\Delta T$ Increases Network Tolerance to Noise

- O-RAN Appendix H, O-DU frequency/time error budget analysis

Table H.2.1 : O-DU Frequency Error Budget

O-DU class	A	B
<ul style="list-style-type: none"> Consider O-DU PTP/SyncE master frequency error budget = (refer to note 1 in clause 11.3.2.1) 	±15 ppb	±5 ppb
<ul style="list-style-type: none"> Consider O-RU total frequency error budget based on O-DU frequency error budget taken away from the 3GPP air interface (±50ppb) budget = 	±35ppb	±45ppb
<ul style="list-style-type: none"> Further split the O-RU total frequency error budget as follows as an example of O-RU design: <ul style="list-style-type: none"> FFO (O-RU subordinate clock) = FFO (O-RU internal additive frequency noise) = 	±21ppb ±14ppb.	±27ppb ±18ppb
<ul style="list-style-type: none"> With FFO (O-RU subordinate clock) value and filter BW = 75mHz, based on ITU-T SG15 Q13 C1730, Geneva, 5 – 16 December 2011: <p style="text-align: center;">$FFO \text{ (in ppb)} = \pm 2 * \pi * dTE_{L+H} \text{ (in ns)} * \text{filter BW (in Hz)}$</p> <ul style="list-style-type: none"> ⇒ FFO (O-RU subordinate clock) = $2\pi * dTE_{L+H} * \text{filter BW}$ ⇒ $dTE_{L+H} = \text{FFO (O-RU subordinate clock)} / (2\pi * \text{filter BW}) =$ <p>which is the max allowed network noise limit (between O-DU UNI and O-RU UNI) guaranteeing FFO at the output of the O-RU filter with 75mHz BW.</p> <p>Note that after this network noise limit is agreed in O-RAN spec, it is up to O-RU vendor implementation to select filter BW (not necessarily 75mHz) to trade off the internal budget split between FFO (O-RU subordinate clock) and FFO (O-RU internal additive frequency noise) as long as the O-RU total frequency error budget (±35ppb or ±43ppb) is still met.</p> 	±45ns	±57ns

- $|dTE_{L+H}| = \pm 45 \text{ ns}$ and $\pm 57 \text{ ns}$ for class A and B, respectively
- Servo loop bw assumed to be 75 mHz, but left to O-RU implementor
- Lower $\Delta F/\Delta T$, lower bw → filters more PDV, can increase unfiltered network noise limit

O-RAN-WG4.CUS.0-v08.00

Real-world Conditions Require Environmentally-resilient Oscillators

More Important

Real-world Use Case	Environmental Stressor	Critical Oscillator Parameter
Radio traffic variation, bursts	Thermal gradient (PCB)	Frequency over temperature slope ($\Delta F/\Delta T$)
Rain shower, cold front	Thermal gradient (ambient)	
Wind, passing vehicles (train, etc.)	Shock, vibration	g (acceleration) sensitivity
Lose upstream frequency ref	-	Allan deviation, holdover

Less Important

Parameter

Banner datasheet spec for Lifetime Freq-over-Temp Stability (e.g. ± 100 ppb) – Not applicable

Conclusion – Proper Oscillator Selection Improves Network Performance

- No impact on PTP time error
 - An oscillator's rated lifetime frequency stability
- Great impact on PTP time error
 - Oscillator $\Delta F/\Delta T$
 - Loop configuration
 - Thermal profile greatly
- Reduce $\Delta F/\Delta T$ to
 - increase time accuracy or
 - increase # of fronthaul hops



Thank You